

# **Physical Optics and Diffraction**

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# Outline

- Physical optics and Kirchhoff Integral
- Diffraction by an aperture
- Fraunhofer diffraction
- Fresnel diffraction
- Image formation
- Dealing with imperfections

# Kirchhoff integral

- Monochromatic scalar wave  $\Psi = \psi(\mathbf{x})e^{-i\omega t}$

with spatial part satisfying *Helmholtz eqn*:

$$\nabla^2 \psi + k^2 \psi = 0$$

for free propagation, eg: one component of **E** field in absence of polarization coupling

- Assume medium is homogeneous and non-dispersive so that  $k$  is constant
- Helmholtz eqn is a *linear, elliptic PDE*, so solution inside a volume is completely determined by value of  $\psi(\mathbf{x})$  and its normal derivative on the boundary.



# Kirchhoff integral (cont..)

- Nice trick available!
- Greens' theorem: for any two (reasonable) scalar functions

$$\int_{\text{boundary}} (\psi \nabla \psi_0 - \psi_0 \nabla \psi) \cdot d\Sigma = - \int_V (\psi \nabla^2 \psi_0 - \psi_0 \nabla^2 \psi) dV$$

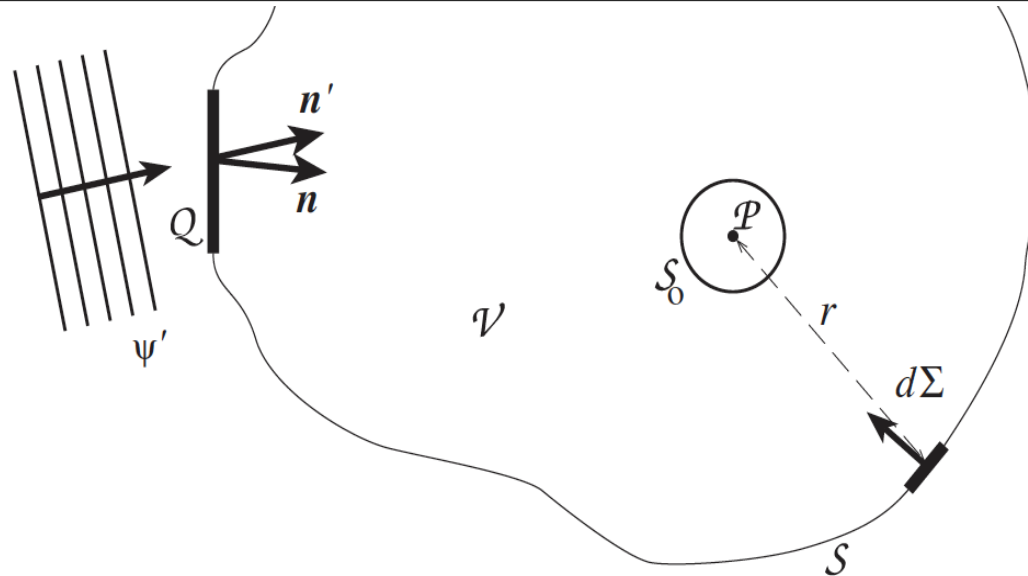
- Above integrals  $\equiv 0$  if both functions satisfy Helmholtz equation
- By inspection  $\psi_0 = \frac{e^{ikr}}{r}$  is a solution

# Kirchhoff integral (cont..)

$$\int_{\text{boundary}} (\psi \nabla \psi_0 - \psi_0 \nabla \psi) \cdot d\Sigma = - \int_V (\psi \nabla^2 \psi_0 - \psi_0 \nabla^2 \psi) dV = 0$$

- With  $\psi_0 = \frac{e^{ikr}}{r}$ , have  $\psi \nabla \psi_0 - \psi_0 \nabla \psi \rightarrow -\psi(0)/r_o^2 + O(1/r_o)$
- So integral over  $S_0$  becomes  $4\pi\psi(\mathcal{P}) \equiv 4\pi\psi_{\mathcal{P}}$
- Therefore

$$\psi_{\mathcal{P}} = \frac{1}{4\pi} \int_S \left( \psi \nabla \frac{e^{ikr}}{r} - \frac{e^{ikr}}{r} \nabla \psi \right) \cdot d\Sigma .$$



# Diffraction by an aperture

- Suppose we have an aperture, which is big compared to the wavelength, but small compared to the distance to  $\mathcal{P}$ . Illumination comes from a *distant* wave source.
- Characterize aperture by a complex function  $t$ , such that the wave just after passing through it  $\psi_Q = t \psi'$
- On the aperture have  $kr \gg 1$ , so write  
 $\nabla(e^{ikr}/r) \simeq -ik\mathbf{n}e^{ikr}/r$ ,  $\mathbf{n}$  pointing towards  $\mathcal{P}$   
 $\nabla\psi \simeq ik t \mathbf{n}' \psi'$ , with  $\mathbf{n}'$  parallel to  $\mathbf{k}$



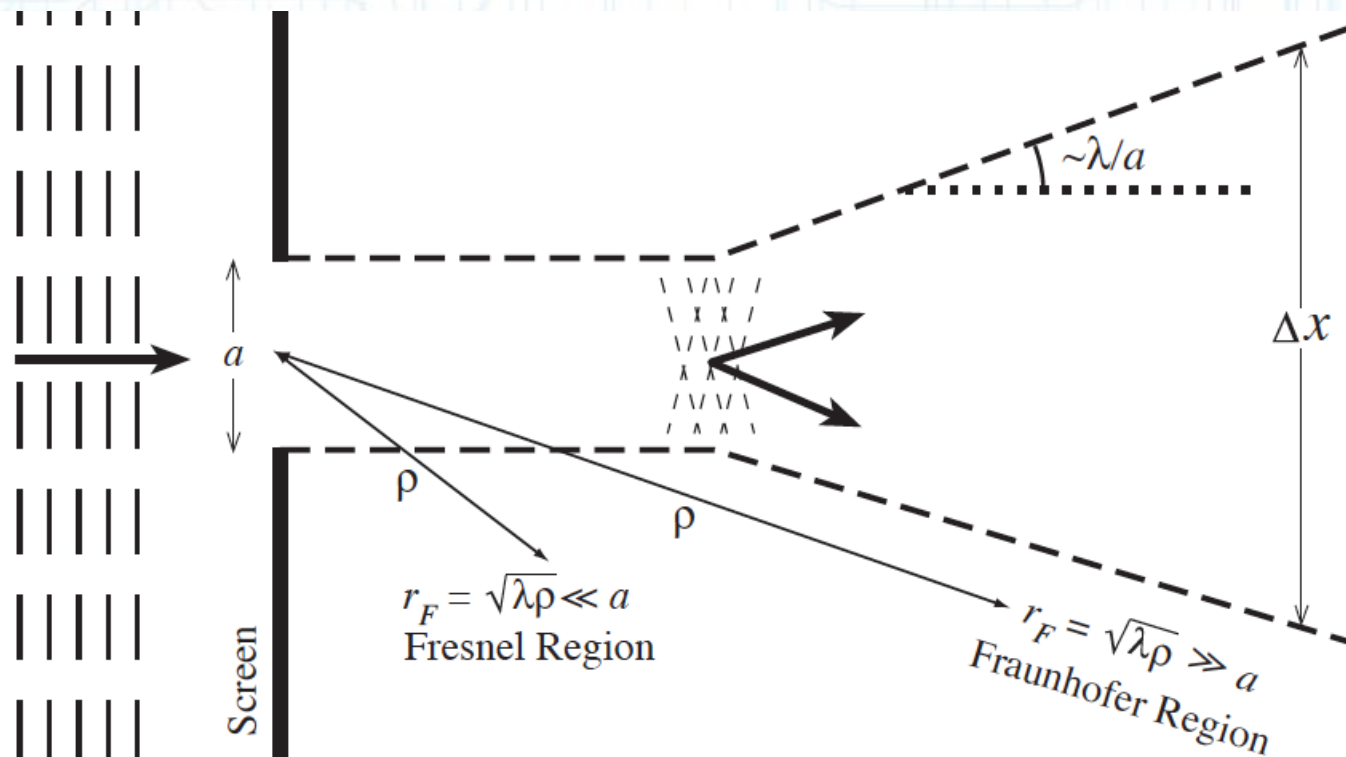
# Diffraction by an aperture

Then

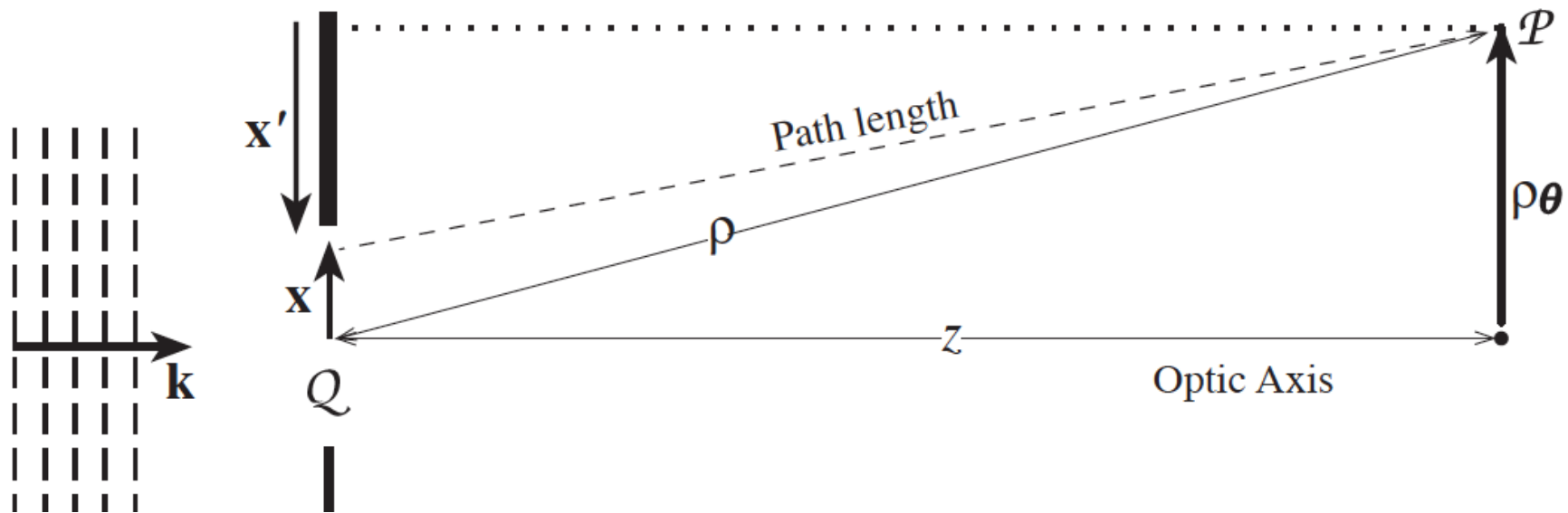
$$\psi_{\mathcal{P}} = -\frac{ik}{2\pi} \int_Q d\Sigma \cdot \left( \frac{\mathbf{n} + \mathbf{n}'}{2} \right) \frac{e^{ikr}}{r} \psi'.$$

Can solve in two different regimes:

- Far field (*Fraunhofer*)
- Near field (*Fresnel*)



# Fraunhofer regime (far field)



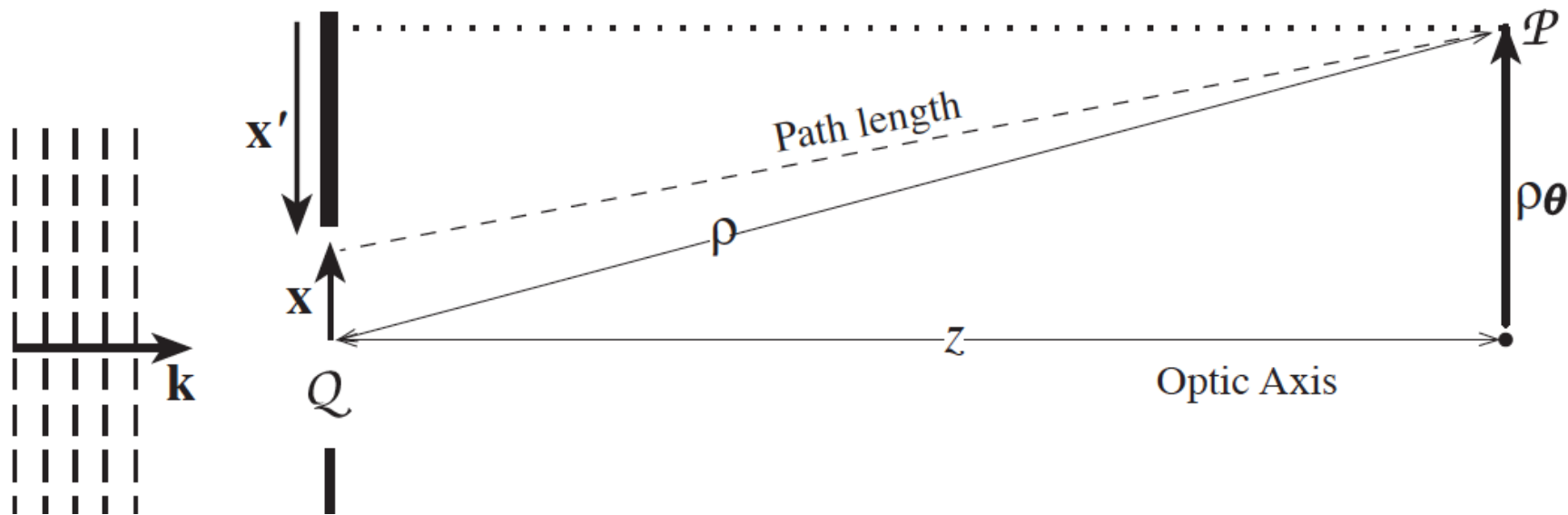
$$\text{Path length} = r = (\rho^2 - 2\rho \mathbf{x} \cdot \boldsymbol{\theta} + x^2)^{1/2} \simeq \rho - \mathbf{x} \cdot \boldsymbol{\theta} + \frac{x^2}{2\rho} + \dots$$

Condition for Fraunhofer is that we can neglect the quadratic phase variation with position in the aperture plane

i.e.  $k \frac{x^2}{2\rho} \ll 1$  for all  $x$ , or  $a \ll \sqrt{\lambda\rho}$



# Fraunhofer regime (far field)



$$\text{Path length} = r = (\rho^2 - 2\rho \mathbf{x} \cdot \boldsymbol{\theta} + x^2)^{1/2} \simeq \rho - \mathbf{x} \cdot \boldsymbol{\theta} + \frac{x^2}{2\rho} + \dots$$

Neglecting the quadratic term:

$$\psi_{\mathcal{P}}(\boldsymbol{\theta}) \propto \int e^{-ik\mathbf{x} \cdot \boldsymbol{\theta}} t(\mathbf{x}) d\Sigma \equiv \tilde{t}(\boldsymbol{\theta}) ,$$

The *amplitude* of the *Fraunhofer* diffraction pattern is given by the **2D Fourier transform** of the aperture function

# Fraunhofer examples

- **Diffraction by a single, finite slit**

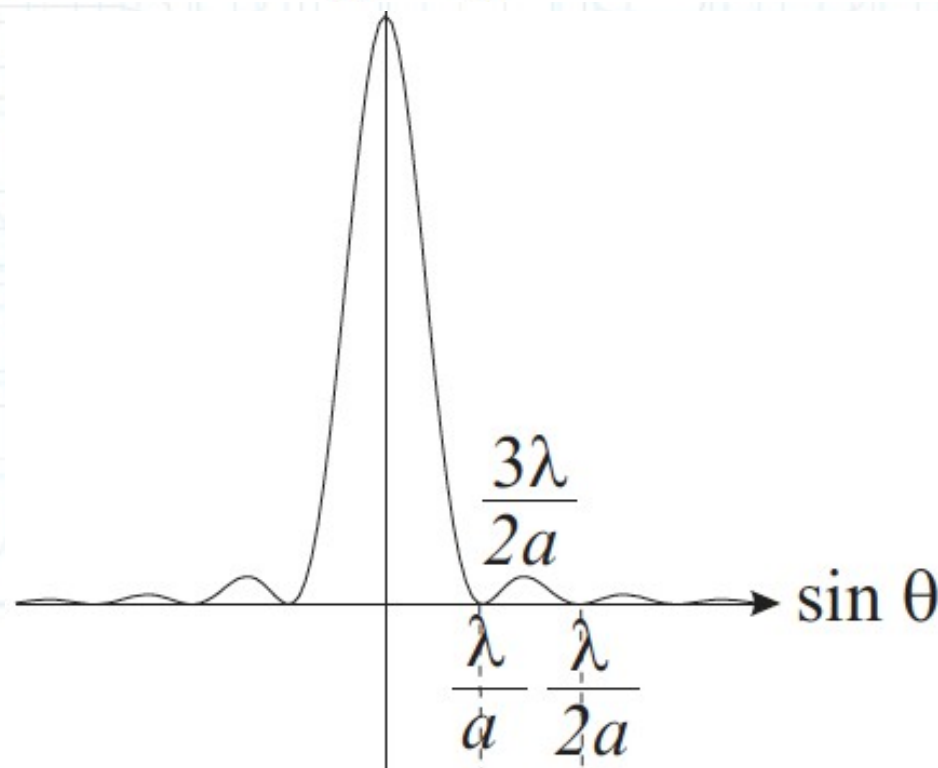
$$t(x) = H_1(x) \equiv \begin{cases} 1 & |x| < a/2 \\ 0 & |x| > a/2 \end{cases}$$

$$\psi_{\mathcal{P}}(\theta) \propto \tilde{H}_1 \propto \int_{-a/2}^{a/2} e^{ikx\theta} dx \propto \text{sinc}\left(\frac{1}{2}ka\theta\right)$$

Then

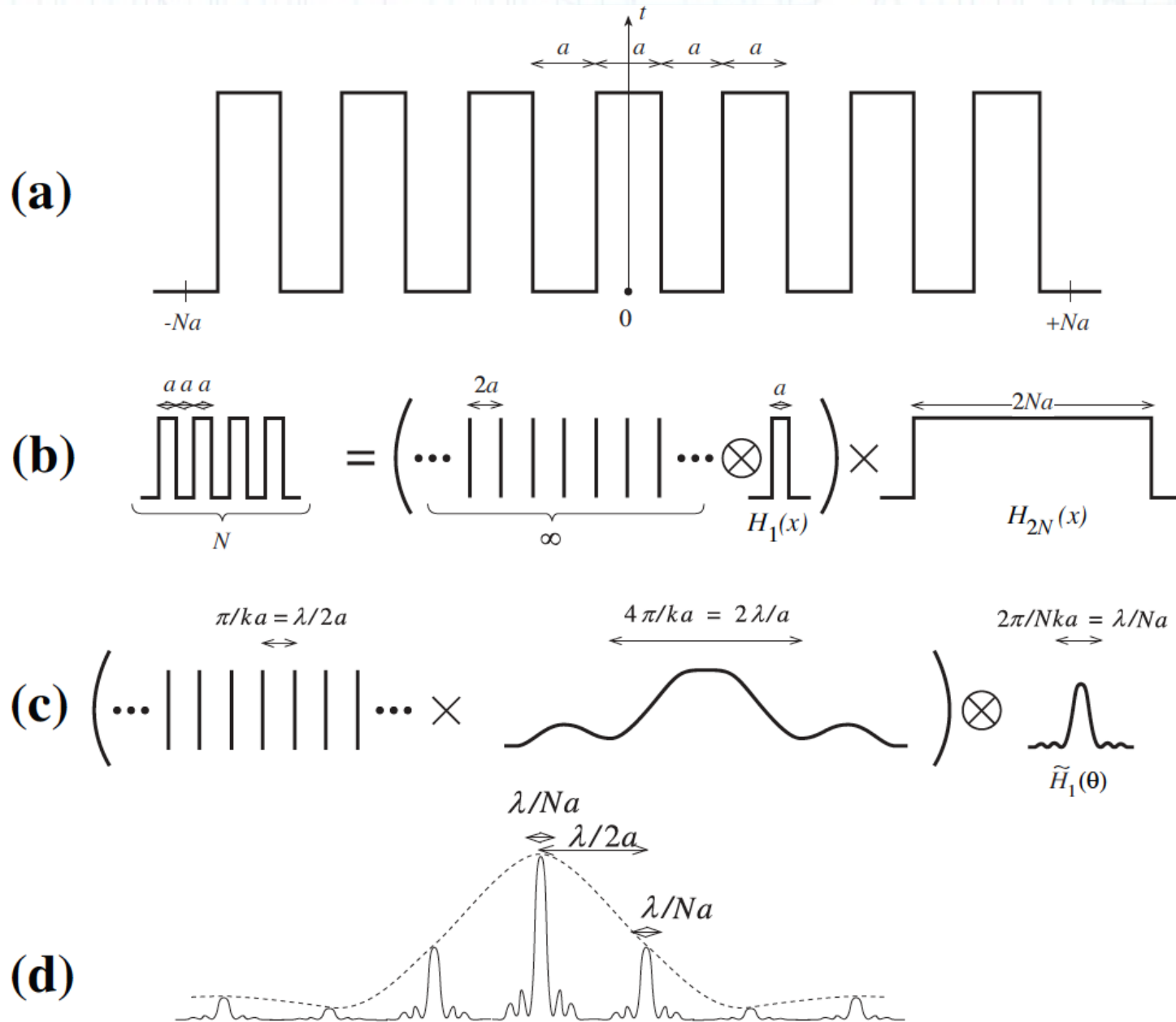
$$F(\theta) \propto \text{sinc}^2\left(\frac{1}{2}ka\theta\right) .$$

Intensity



# Fraunhofer examples

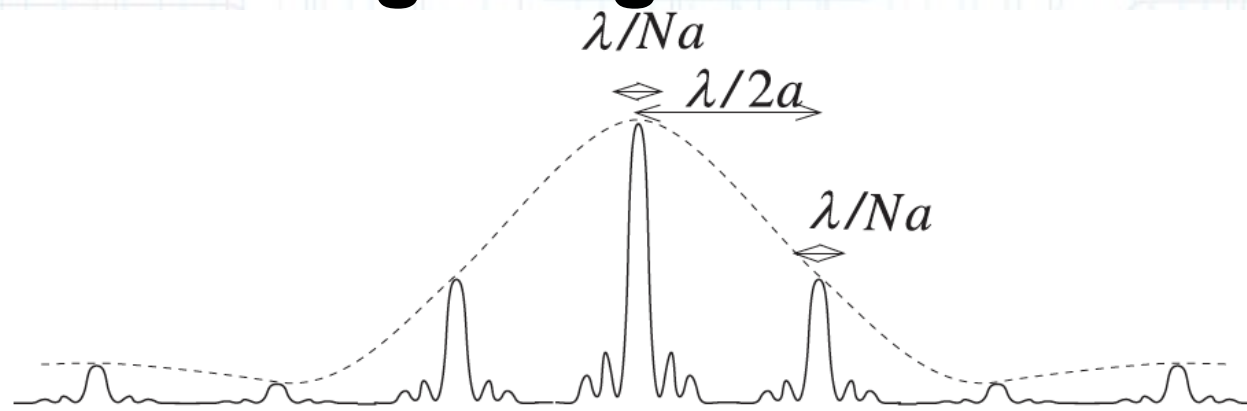
- Diffraction grating



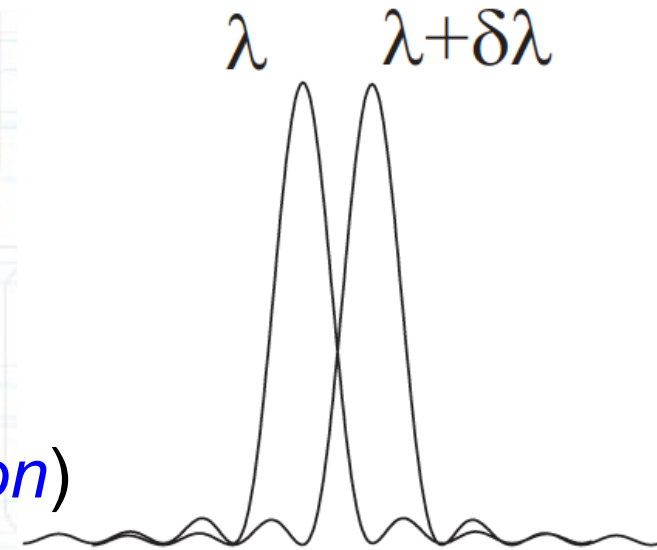


# Fraunhofer examples

- **Diffraction grating**



- $p$ -th order beam deflected by  $\theta = \pi p / ka = p\lambda / 2a$
- Consider beams for waves at  $\lambda$  and  $\lambda + \delta\lambda$
- Located at  $\theta = p\lambda / 2a$  and  $p(\lambda + \delta\lambda) / 2a$
- Separation  $\delta\theta = p\delta\lambda / 2a$
- Can distinguish them if maximum of one corresponds to first minimum of the other, i.e.  $\delta\theta$  is at least  $\lambda / 2Na$  (*Rayleigh criterion*)
- Corresponds to  $\frac{\lambda}{\delta\lambda} \gtrsim \mathcal{R} \equiv Np$  (*chromatic resolving power*)



# Fraunhofer examples

- **Diffraction by a circular aperture**

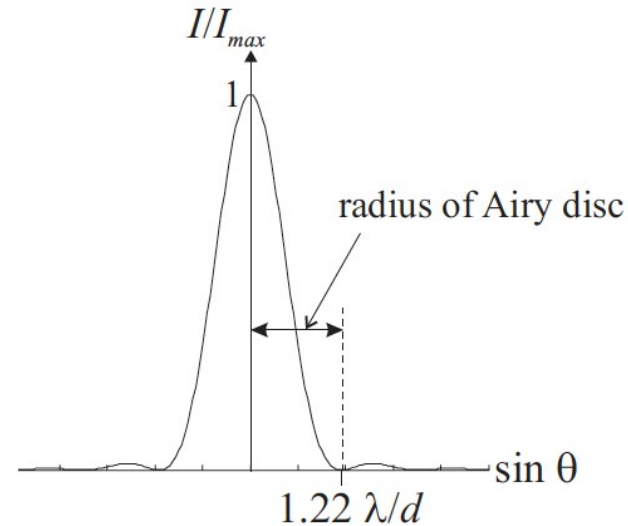
$$\psi(\theta) \propto \int_{\text{Disk with diameter } D} e^{-ik\mathbf{x}\cdot\boldsymbol{\theta}} d\Sigma \propto \frac{J_1(kD\theta/2)}{kD\theta/2}$$

- Most of the light from a distant source falls within the Airy disc

$$\theta_A = 1.22\lambda/D$$

- Can use to calculate the *diffraction limit* of a lens/telescope
- Two equally bright sources can be resolved only if the radius of the Airy disc is less than their separation, i.e if their angular separation is more than

$$\theta_{\min} = \theta_A = 1.22\lambda/D$$



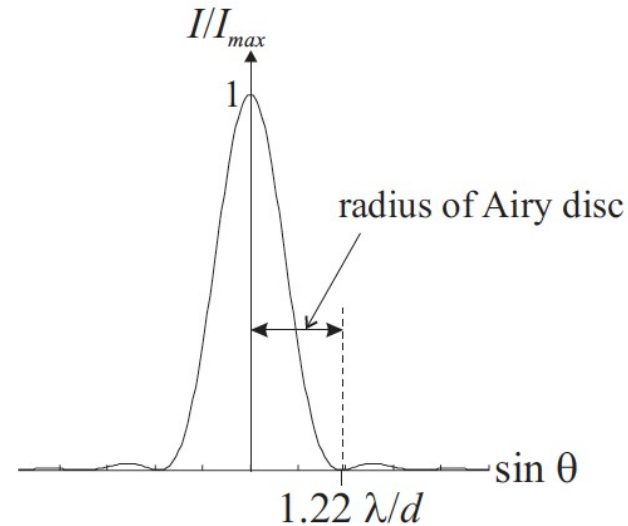
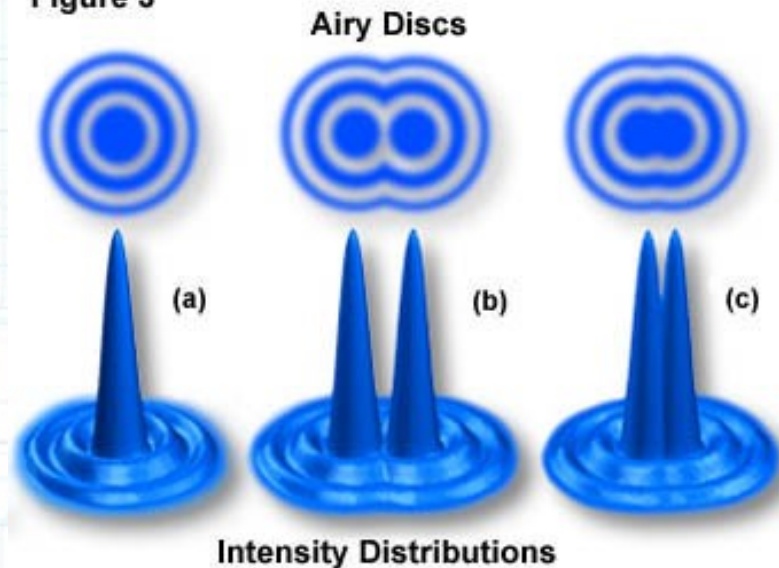


# Fraunhofer examples

- Diffraction by a circular aperture

$$\psi(\theta) \propto \int_{\text{Disk with diameter } D} e^{-ik\mathbf{x}\cdot\boldsymbol{\theta}} d\Sigma \propto \frac{J_1(kD\theta/2)}{kD\theta/2}$$

Figure 3



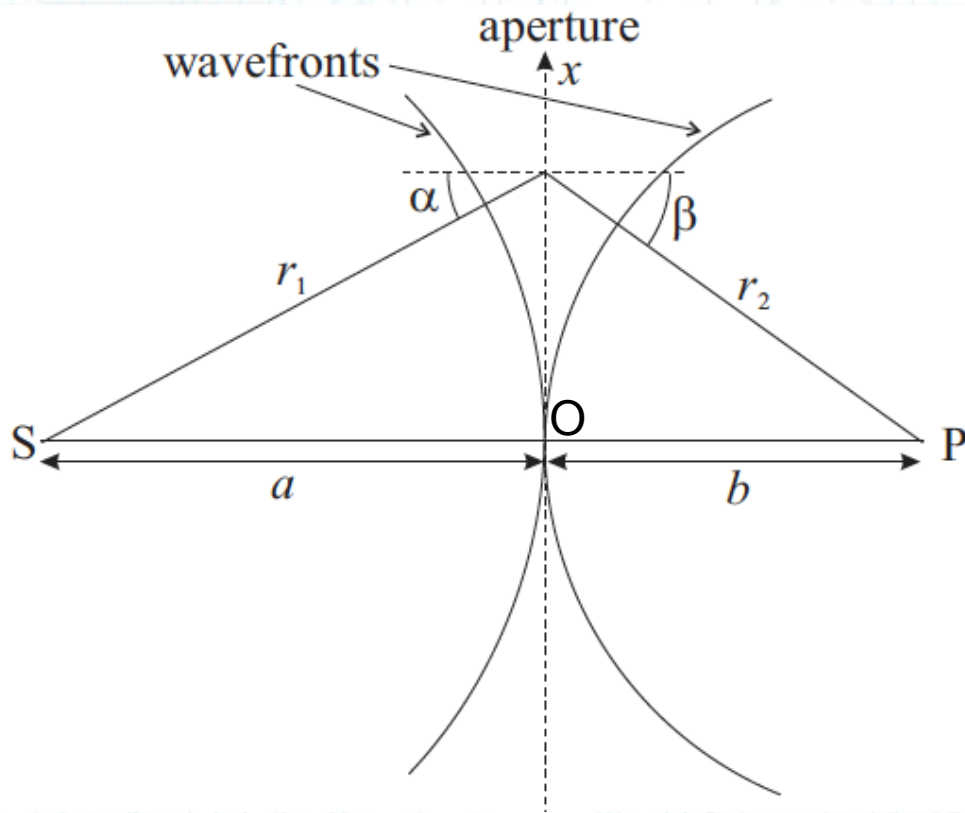
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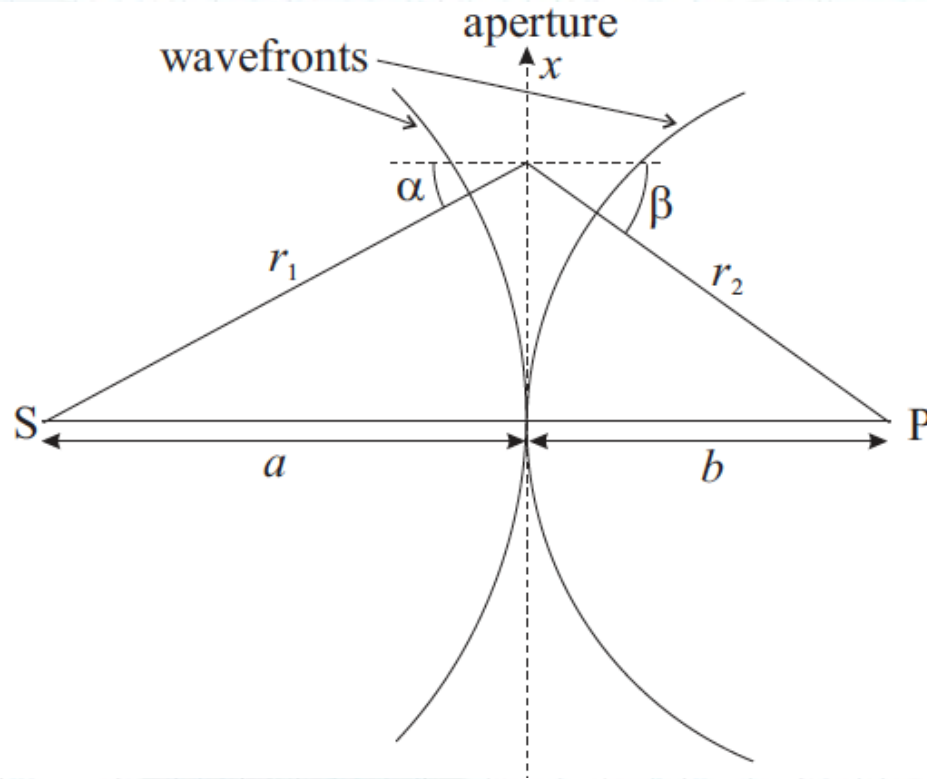
# Fresnel regime (near field)

- Now can't neglect quadratic phase variation
- Problem a bit harder. Consider *special case* in which the source, the origin of coordinates and the observation point are aligned



Might seem  
uninteresting, but  
can make a lot of  
progress by moving  
the origin!

# Fresnel regime (near field)



$$\begin{aligned} r_1 + r_2 &= \sqrt{a^2 + x^2 + y^2} + \sqrt{b^2 + x^2 + y^2} \\ &= a + b + \frac{x^2 + y^2}{2a} + \frac{x^2 + y^2}{2b} \\ &\quad + \text{higher order terms} \end{aligned}$$

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write  $\frac{1}{R} = \frac{1}{a} + \frac{1}{b}$  then optical path = const. +  $\frac{x^2 + y^2}{2R}$

$$\psi_P \propto \int t(x, y) \exp \left( ik \frac{x^2 + y^2}{2R} \right) d\Sigma$$



# Separable aperture

If the aperture function is separable (e.g. rectangular aperture), it is convenient to rewrite in terms of *Fresnel integrals*.

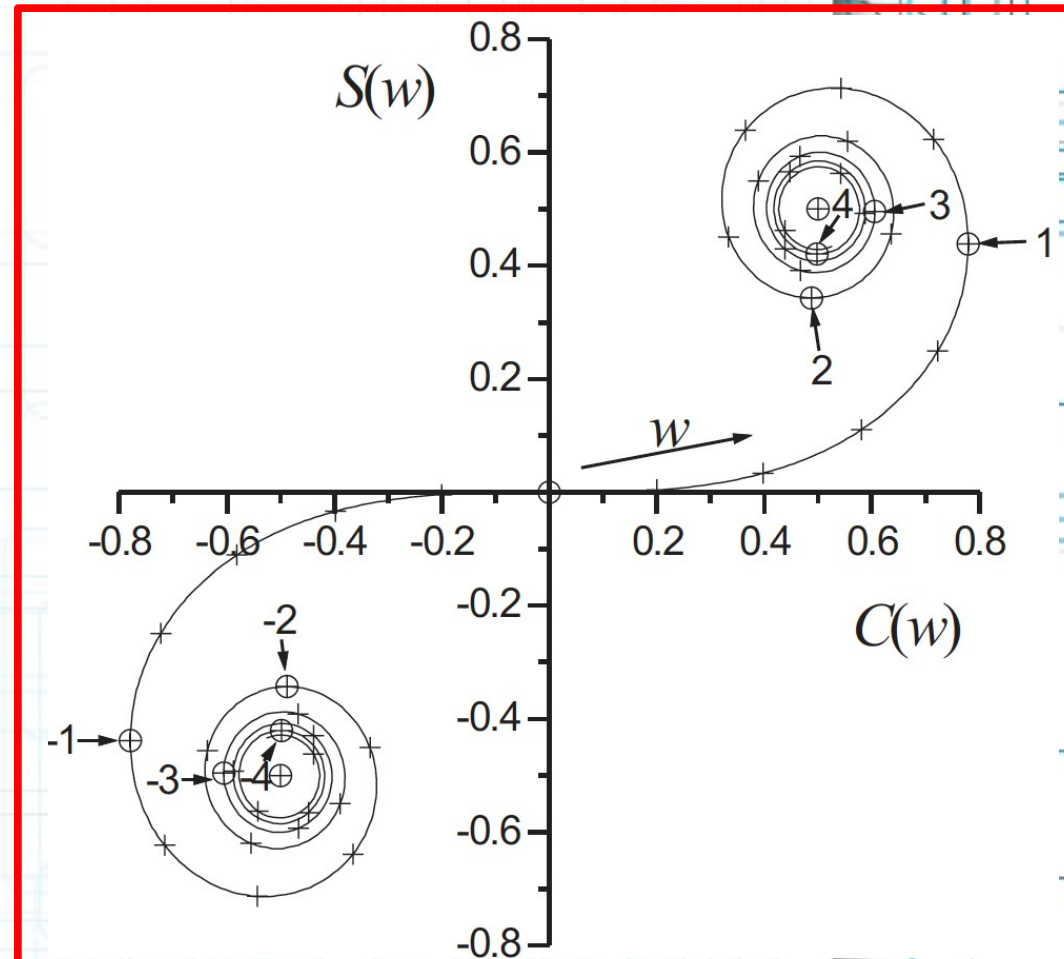
Change variables to  $u = x\sqrt{\frac{2}{\lambda R}} ; v = y\sqrt{\frac{2}{\lambda R}}$

Define **Fresnel integral**

$$\int_0^w \exp\left(\frac{i\pi u^2}{2}\right) du = C(w) + iS(w)$$

Plotting C vs S, obtain the  
**Cornu spiral**

$$C(\infty) = 0.5 \quad S(\infty) = 0.5$$



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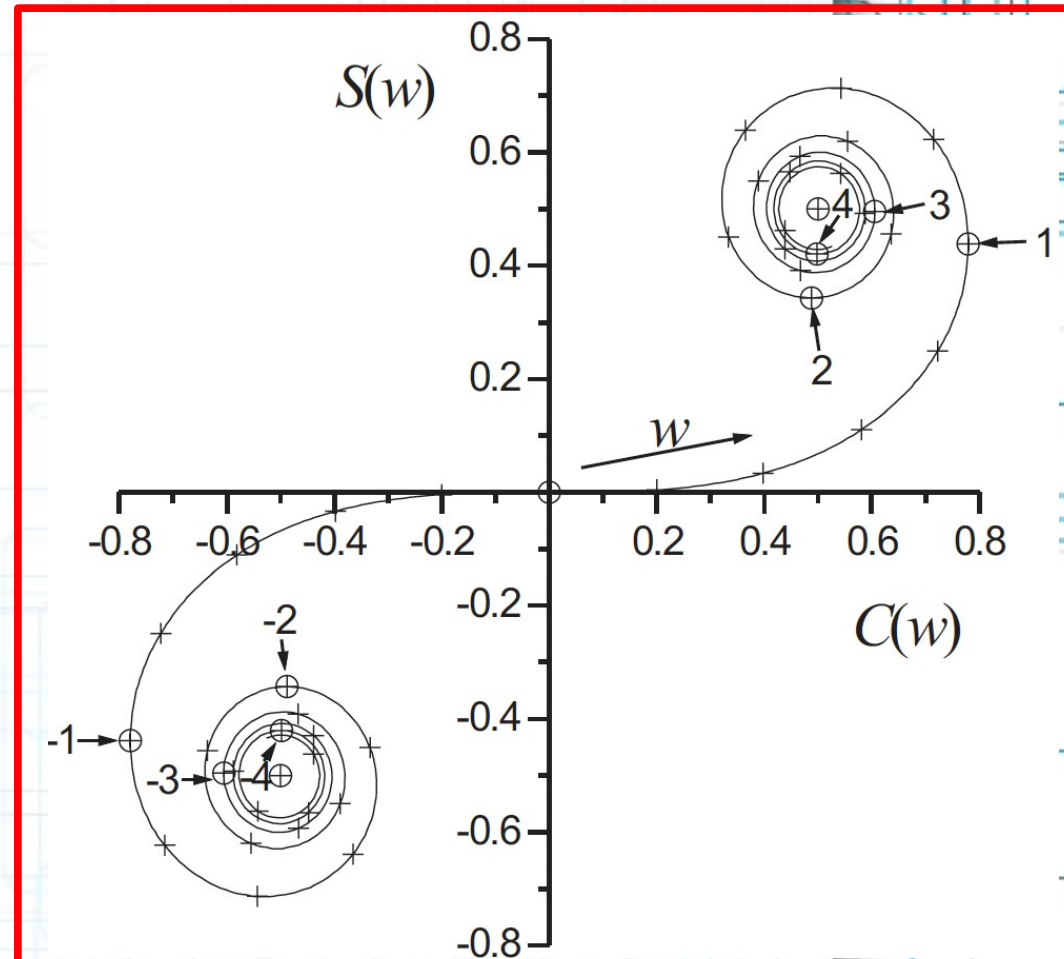
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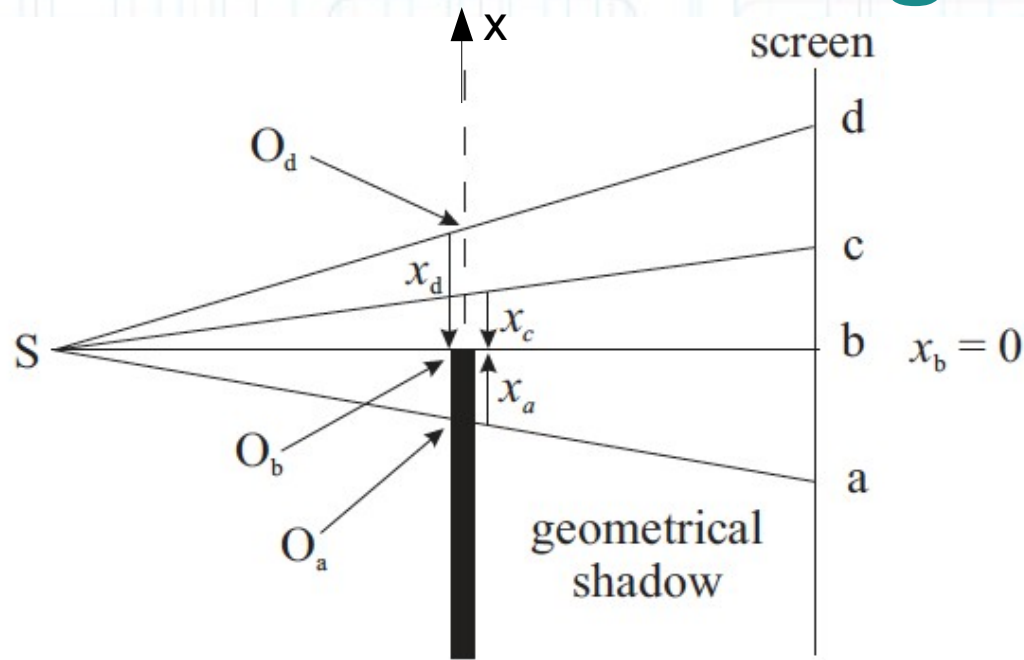
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Plotting C vs S, obtain the  
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$$C(\infty) = 0.5 \quad S(\infty) = 0.5$$



# Diffraction from straight edge



$$\begin{aligned}\psi_P &\propto \int_{x_1}^{x_2} \exp\left(\frac{ikx^2}{2R}\right) dx \propto \int_{w_1}^{w_2} \exp\left(\frac{i\pi u^2}{2}\right) du \\ &= C(w_2) - C(w_1) + i(S(w_2) - S(w_1))\end{aligned}$$

a  $x_2 = \infty \quad x_1 = x_a > 0$

b  $x_2 = \infty \quad x_1 = x_b = 0$

the geometrical edge

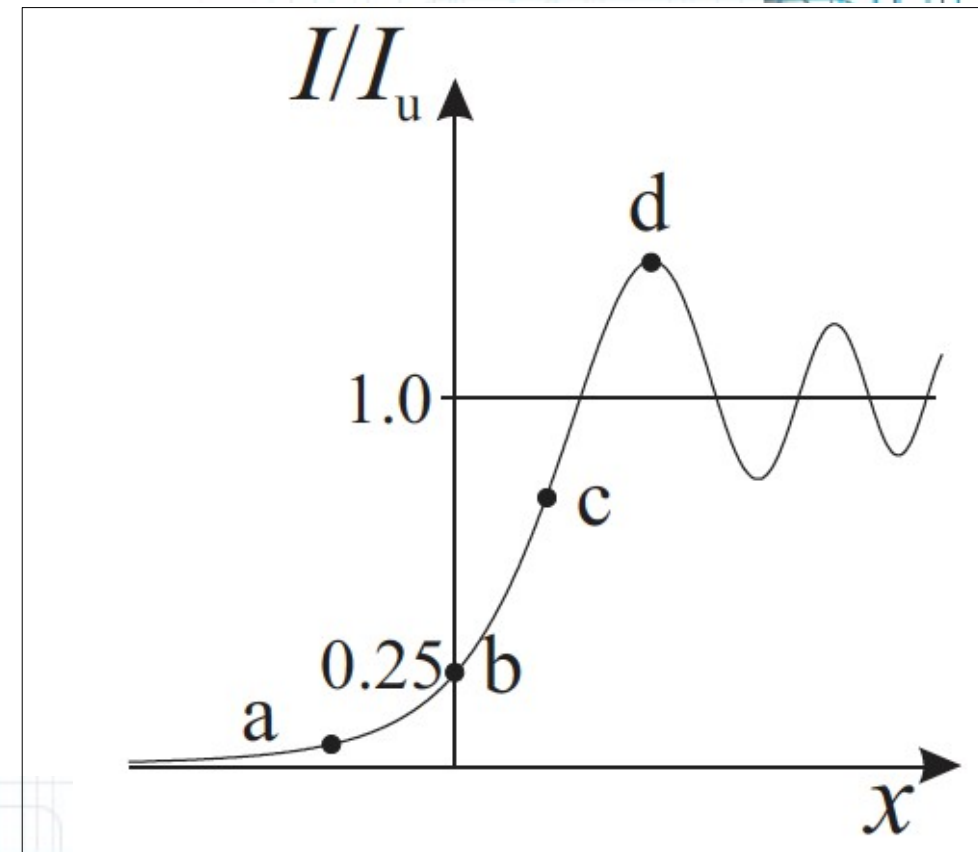
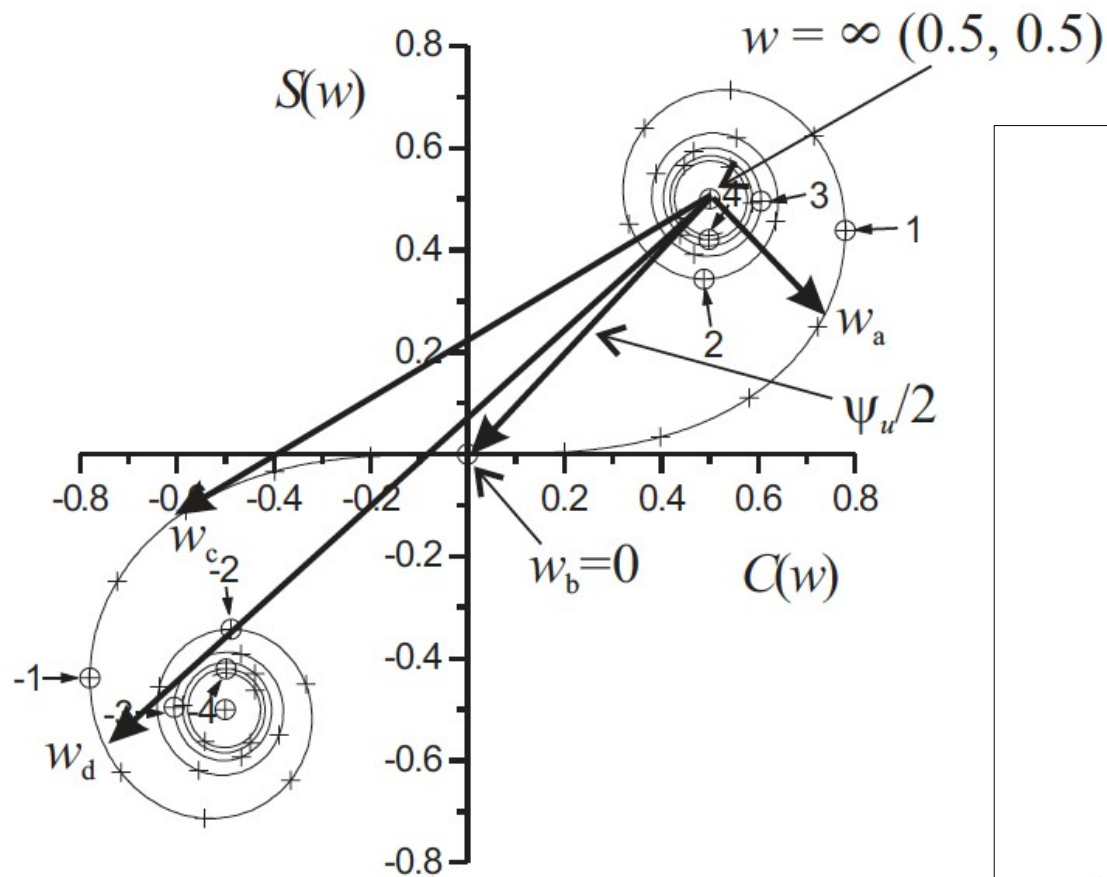
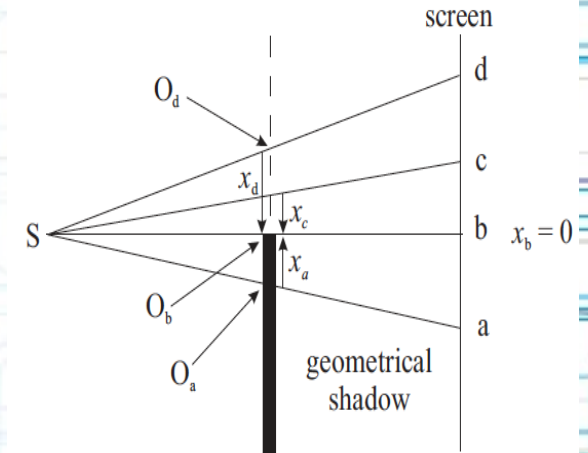
c  $x_2 = \infty \quad x_1 = x_c < 0$

d  $x_2 = \infty \quad x_1 = x_d; w_d \sim -1.26$  maximum  $|\psi_P|$



# Diffraction from straight edge

- a  $x_2 = \infty \quad x_1 = x_a > 0$
  - b  $x_2 = \infty \quad x_1 = x_b = 0$
  - c  $x_2 = \infty \quad x_1 = x_c < 0$
  - d  $x_2 = \infty \quad x_1 = x_d; w_d \sim -1.26$  maximum  $|\psi_P|$
- the geometrical edge

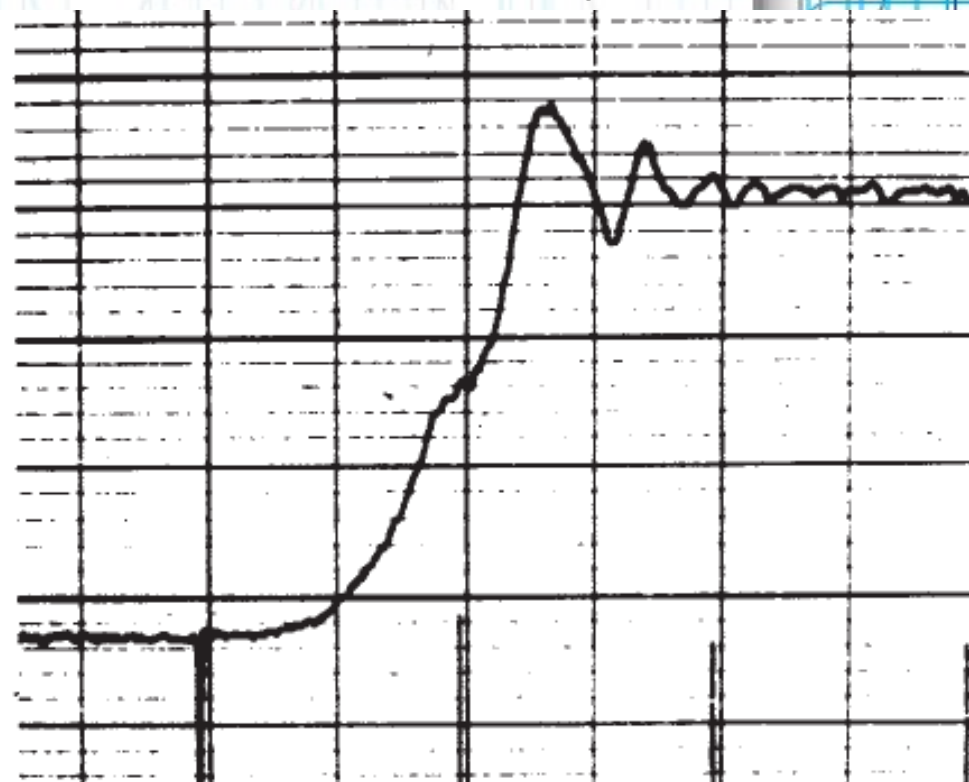
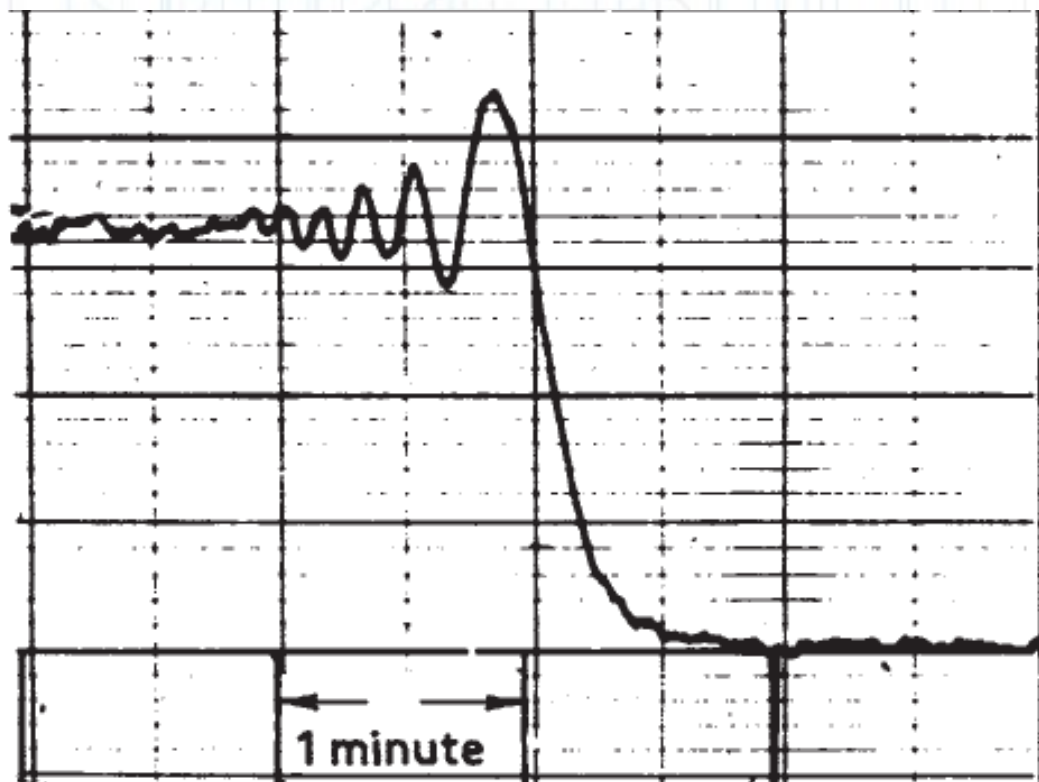


# INVESTIGATION OF THE RADIO SOURCE 3C 273 BY THE METHOD OF LUNAR OCCULTATIONS

By C. HAZARD, M. B. MACKEY and A. J. SHIMMINS

C.S.I.R.O. Division of Radiophysics, University Grounds, Sydney

- Use the Fresnel pattern from lunar occultation of the powerful 3C 273 radio source to determine its position accurately



# Diffraction by circular aperture

- Consider circular aperture w/ radius  $D$
- Retain the obliquity factor  $K$
- Using polar coordinates:

$$\psi_P \propto \int_{\rho=0}^{\rho=D} \frac{K}{(a^2 + \rho^2)^{1/2}(b^2 + \rho^2)^{1/2}} \exp\left(\frac{ik\rho^2}{2R}\right) 2\pi\rho d\rho.$$

- Use the substitution  $\rho^2 = s$  ;  $2\rho d\rho = ds$

$$\psi_P \propto \int_{s=0}^{s=D^2} \frac{K}{(a^2 + s)^{1/2}(b^2 + s)^{1/2}} \exp\left(\frac{i\pi s}{\lambda R}\right) \pi ds$$

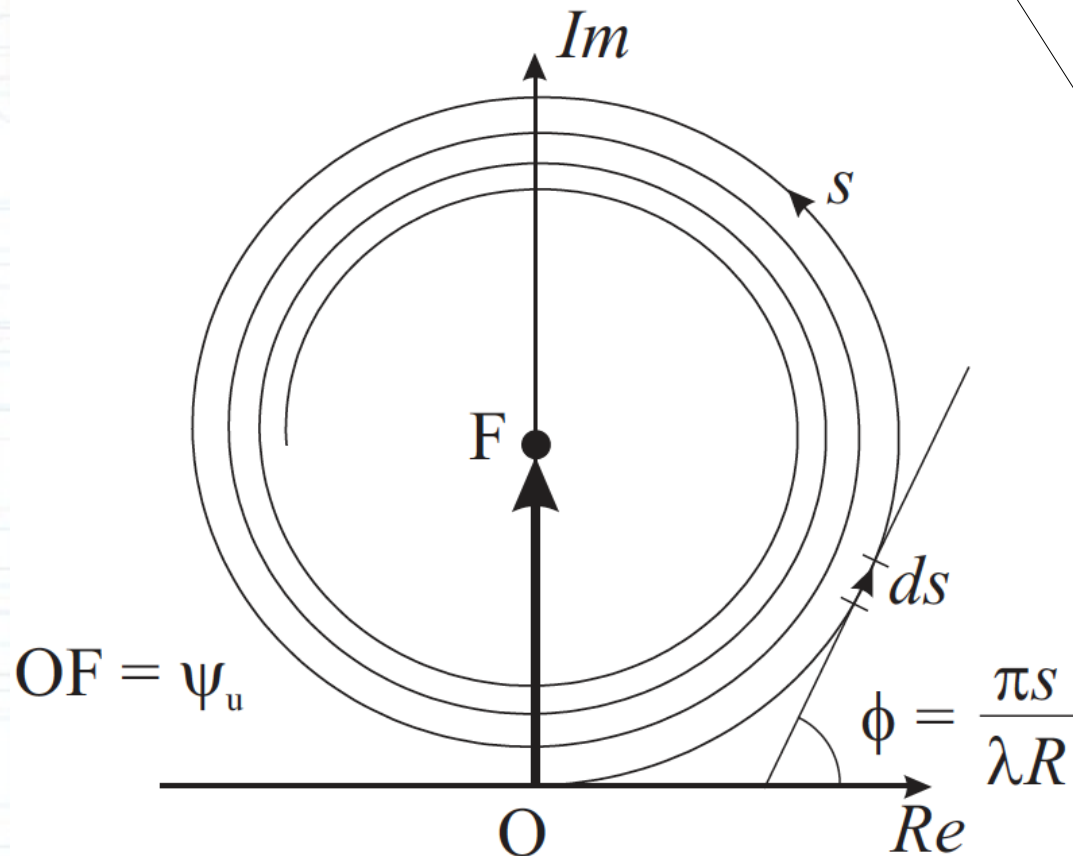
- **Note:** only valid on axis!



# Diffraction by circular aperture

$$\psi_P \propto \int_{s=0}^{s=D^2} \frac{K}{(a^2 + s)^{1/2}(b^2 + s)^{1/2}} \exp\left(\frac{i\pi s}{\lambda R}\right) \pi ds$$

- Evaluate graphically



Going around in a circle

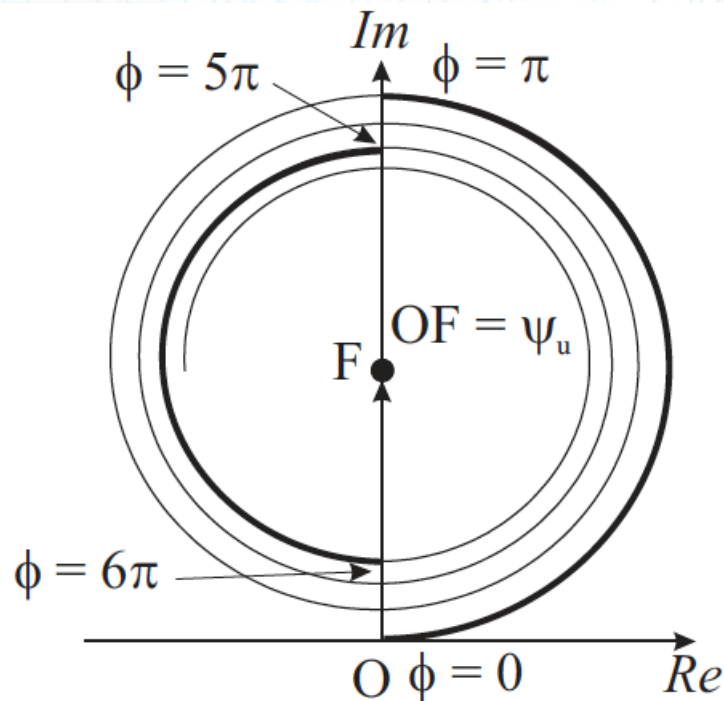
Spiralling in

# Diffraction by circular aperture and Fresnel Zones

For finite apertures, the diffraction integral varies considerably

$$\begin{aligned} \phi = 2n\pi & \quad \rho^2 = 2n\lambda r & \Rightarrow \psi \approx 0 \\ \phi = (2n+1)\pi & \quad \rho^2 = (2n+1)\lambda r & \Rightarrow \psi \approx 2\psi_u \end{aligned}$$

Define Fresnel zones as concentric rings in the aperture plane over which the phase varies at the observation point varies by  $\pi$



1<sup>st</sup> zone:  $0 \leq \phi(\rho) \leq \pi$   
 $\rho^2 \leq \lambda R.$

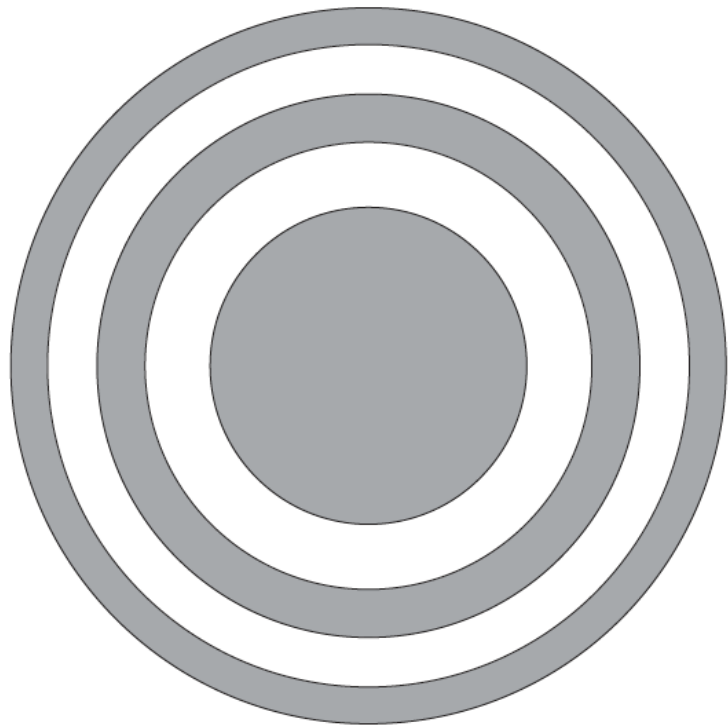
Nth zone:  $(n-1)\pi \leq \phi(\rho) \leq n\pi$   
 $\sqrt{(n-1)\lambda R} \leq \rho \leq \sqrt{n\lambda R}.$

**Note:** Area of each zone is the same  $\pi (\rho_n^2 - \rho_{n-1}^2) = \pi \lambda R.$

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$$\begin{aligned} \text{1}^{\text{st}} \text{ zone:} \quad & 0 \leq \phi(\rho) \leq \pi \\ & \rho^2 \leq \lambda R. \end{aligned}$$

$$\begin{aligned} \text{Nth zone:} \quad & (n-1)\pi \leq \phi(\rho) \leq n\pi \\ & \sqrt{(n-1)\lambda R} \leq \rho \leq \sqrt{n\lambda R}. \end{aligned}$$

**Note:** Area of each zone is the same  $\pi (\rho_n^2 - \rho_{n-1}^2) = \pi \lambda R.$



# Diffraction by circular aperture and Fresnel Zones

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*Odd* numbered zones *add* to, and *even* numbered zones *subtract* from the overall amplitude at P.

So, for an observation point P on the optic axis of a circular aperture of radius  $a$ , the aperture includes  $N$  zones, given by  $a^2 = n\lambda R$ .

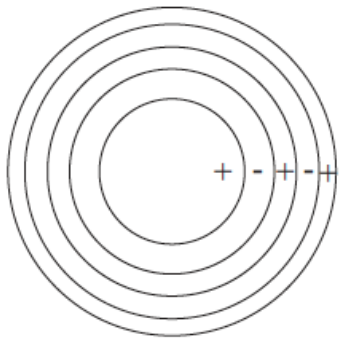
N ODD: bright spot at P;  $\psi \sim 2\psi_u$ ;  $I \sim 4I_u$

N EVEN: dark spot at P:  $\psi \sim 0$ ;  $I \sim 0$

# Zone plate

- A **Fresnel zone plate** is an aperture that blocks alternates half-period zones.
- Eg: block the *odd* ones

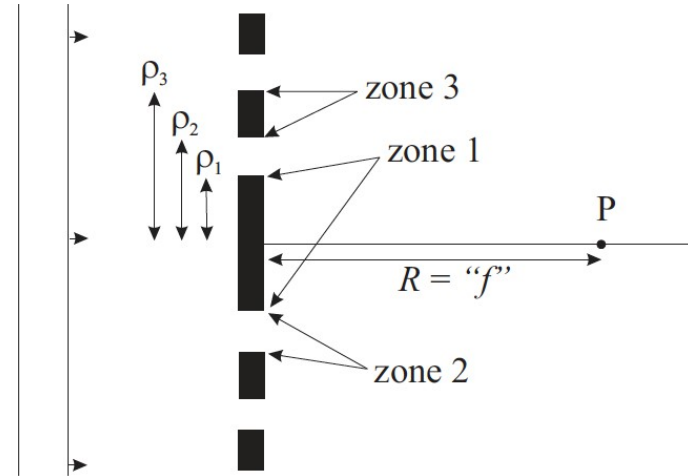
Fresnel Zones



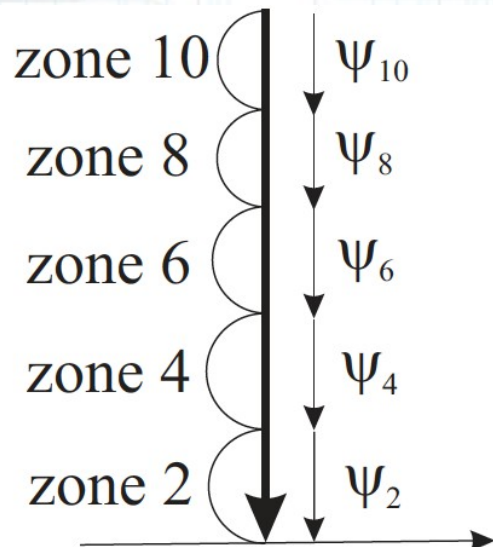
Zone plate



wavefronts



$$\rho_1 = \sqrt{\lambda R}, \quad \rho_2 = \sqrt{2\lambda R}, \quad \rho_3 = \sqrt{3\lambda R}, \quad \text{etc}$$



Net amplitude at  $P$ :

$$\begin{aligned} \psi_P &= \psi_2 + \psi_4 + \psi_6 + \dots \\ &\approx 2N\psi_u \end{aligned}$$

Intensity  $I_P \approx 4N^2 I_u$

Incident wave brought to focus at P!  
Acts like a **lens** of focal length

$$f = \frac{\rho_1^2}{\lambda} = \frac{\rho_n^2}{n\lambda}$$



# Zone plate (cont..)

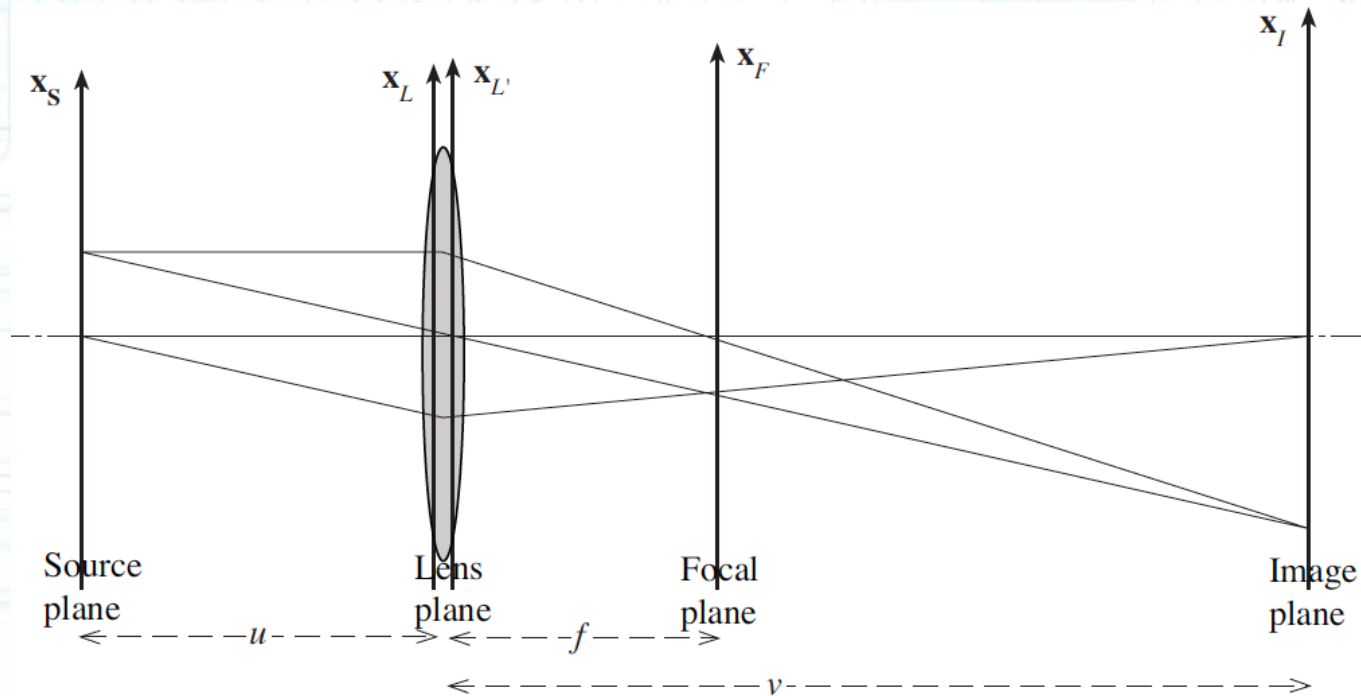
- $f \propto 1/\lambda \rightarrow$  highly chromatic lens
- Focuses different wavelengths in different foci
- Works for any frequency (including X-rays)
- Maximum resolution depends on smallest zone width





# Image formation (thin lens)

- Field at distance  $z_j$  along the optical axis:  $\psi_j(\mathbf{x})$
- Vector  $\mathbf{x}$  is perpendicular to the optic axis
- For a linear system 
$$\psi_2(\mathbf{x}_2) = \int P_{21}(\mathbf{x}_2, \mathbf{x}_1) d\Sigma_1 \psi_1$$
- $P_{21}$  is the *propagator* or *Point Spread Function* (PSF)



# Image formation (thin lens)

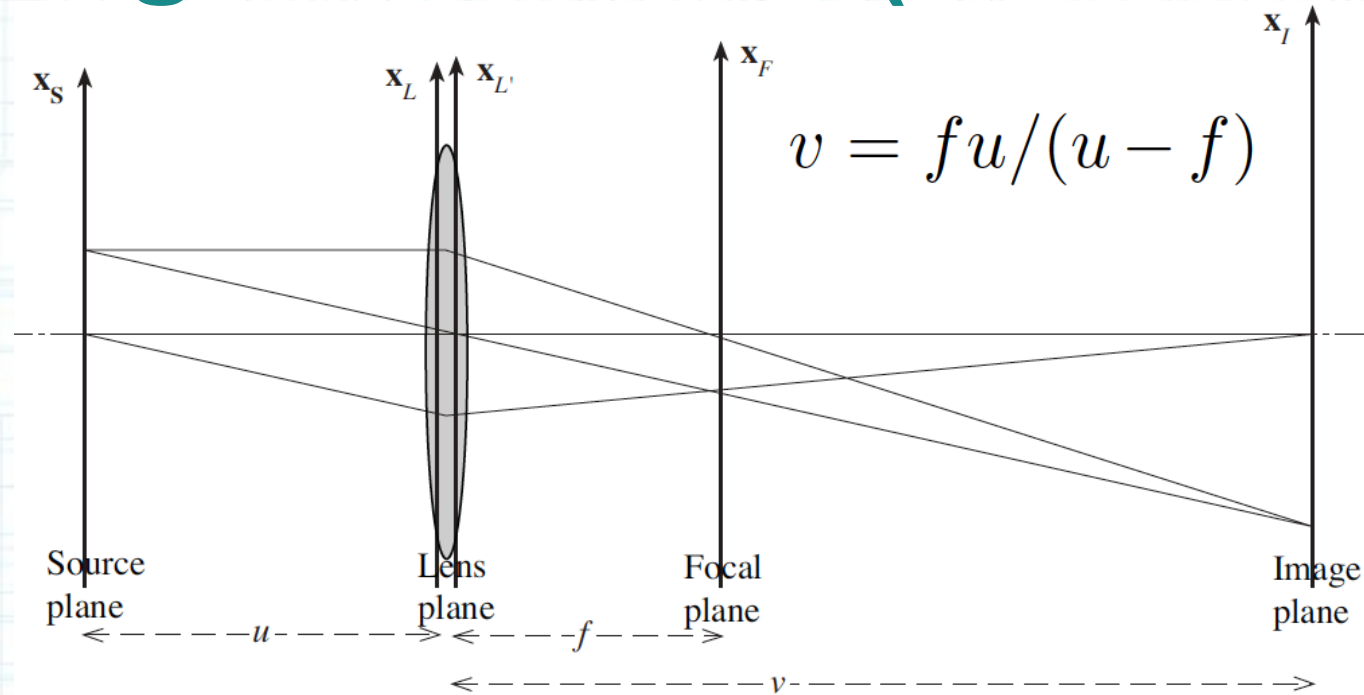
- Field at distance  $z_j$  along the optical axis:  $\psi_j(\mathbf{x})$
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- $P_{21}$  is the *propagator* or *Point Spread Function* (PSF)
- **Free propagation** through  $d = z_2 - z_1$

$$P_{21} = \frac{-ik}{2\pi d} e^{ikd} \exp\left(\frac{ik(\mathbf{x}_1 - \mathbf{x}_2)^2}{2d}\right)$$

- **Thin lens**: phase shift depends quadratically on the distance from optic axis  $|\mathbf{x}|$

$$P_{21} = \exp\left(\frac{-ik|\mathbf{x}_1|^2}{2f}\right) \delta(\mathbf{x}_2 - \mathbf{x}_1)$$

# Image formation (thin lens)



- Propagating to the *focal plane*:

$$\begin{aligned}
 P_{FS} &= \int P_{FL'} d\Sigma_{L'} P_{L'L} d\Sigma_L L P_{LS} \\
 &= \int \frac{ik}{2\pi f} e^{ikf} \exp\left(\frac{ik(\mathbf{x}_F - \mathbf{x}_{L'})^2}{2f}\right) d\Sigma_{L'} \delta(\mathbf{x}_{L'} - \mathbf{x}_L) \exp\left(\frac{-ik|\mathbf{x}_L|^2}{2f}\right) \\
 &\quad \times d\Sigma_L \frac{-ik}{2\pi u} e^{iku} \exp\left(\frac{ik(\mathbf{x}_L - \mathbf{x}_S)^2}{2u}\right) \\
 &= \frac{-ik}{2\pi f} e^{ik(f+u)} \exp\left(-\frac{ikx_F^2}{2(v-f)}\right) \exp\left(-\frac{ik\mathbf{x}_F \cdot \mathbf{x}_S}{f}\right) .
 \end{aligned}$$



# Image formation (thin lens)

- Propagating from source to the *focal plane*:

$$P_{FS} = \frac{-ik}{2\pi f} e^{ik(f+u)} \exp\left(-\frac{ikx_F^2}{2(v-f)}\right) \exp\left(-\frac{ik\mathbf{x}_F \cdot \mathbf{x}_S}{f}\right)$$

- Amplitude given by  $\psi_F(\mathbf{x}_F) = \int P_{FS} d\Sigma_S \psi_S(\mathbf{x}_S)$

$$\psi_F(\mathbf{x}_F) = -\frac{ik}{2\pi f} e^{ik(f+u)} \exp\left(-\frac{ikx_F^2}{2(v-f)}\right) \tilde{\psi}_S(\mathbf{x}_F/f) .$$

- Therefore the amplitude in the *focal plane* is proportional to the **Fourier transform** of the field in the *source plane*
- Focal plane can be used for *spatial filtering*, i.e. processing the image by altering its Fourier transform

# Image formation (thin lens)

- Finally, free propagation from focal plane to image plane

$$\psi_I = \int P_{IF} d\Sigma_F \psi_F$$

$$\psi_I(\mathbf{x}_I) = - \left( \frac{u}{v} \right) e^{ik(u+v)} \exp \left( \frac{ikx_I^2}{2(v-f)} \right) \psi_S(\mathbf{x}_S = -\mathbf{x}_I u/v) .$$

- Apart from a phase factor, the field in the image plane is just a magnified version of the original field, with the correct magnification
- Theory due to E. Abbe (1873)



# Dealing with imperfections...

- So far only considered perfect lenses/mirrors and uniform propagation medium
- When any of the above assumptions fail, the image quality is degraded
- Useful to define the **Strehl ratio** as the ratio between the peak amplitude of the actual PSF and the peak amplitude expected in the presence of diffraction only
- Looking through the atmosphere, the Strehl ratio will be very low, even with good optics (due to atmospheric turbulence).
- In presence of *Adaptive Optics* systems, can get very close to 1 (diffraction limited)



# Dealing with imperfections...

- Can treat aberrations and imperfections in the physical optics language (but it's a hard problem, see Born & Wolf)
- Can relate rms imperfection in the optics with actual intensity in the focal plane

$$I_P = I_0 \left[ 1 - \left( \frac{2\pi}{\lambda} \right)^2 (\Delta\Phi)^2 \right]$$

- For example, in order to have  $I_p/I_0 \approx 0.8$   
we need

$$|\Delta\Phi| < \lambda/14$$

# References

- Born & Wolf, *Principles of Optics*
- Hecht, *Optics*
- Blanford & Thorne, *Applications of Classical Physics lecture notes*
- Part IB *Optics lecture notes* (Cambridge)